

# Report on ITER-relevant Scenario Experiments on DIII-D

Presented by  
T.C. Luce

Presented at  
ITPA Integrated Operation Scenarios  
Topical Group Meeting  
Kyoto, Japan

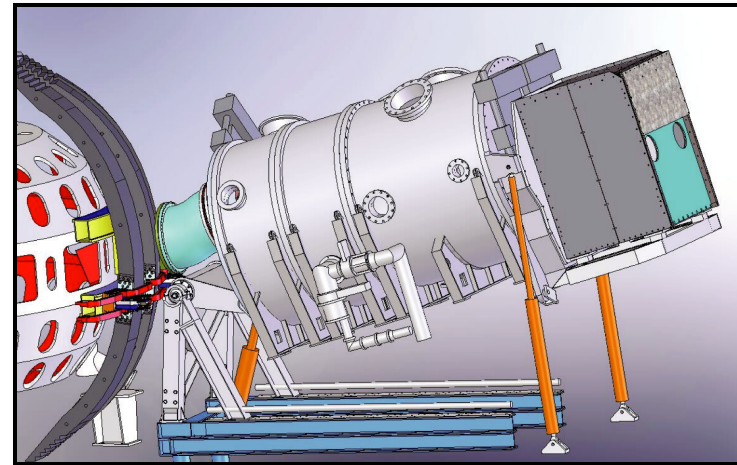
Oct. 18–21, 2011

# What's Here, What's Not

- **Talk tries to cover DIII-D experiments of interest to ITER and potential future joint experiments from the last run (May-Sept.)**
  - Steady-state scenario with off-axis NBI
  - Advanced inductive with low or no external torque input
  - QH mode with no external torque source
  - Divertor characterization
  - Closed-loop demonstration of current profile control with a physics-based model
- **Plans for Oct. run will be shown**
  - Plans for 2012 very uncertain at this point
- **Most, if not all, of the results directly in support of joint experiments will be reported through the joint experiment spokespersons**

# Steady State Scenario Work Focused on $\min(q) > 2$ with Off-axis NBI

- Previous attempts to probe the  $\beta$  limit with  $\min(q) > 2$  found central co-NBI overdrove the central current at the powers needed
  - Insufficient power at higher B
- Theoretical and experimental studies indicated higher  $\beta$  limits when the pressure and current profiles were broader
- Both considerations motivated modifying 1 beamline in DIII-D to tilt vertically to give off-axis NBI



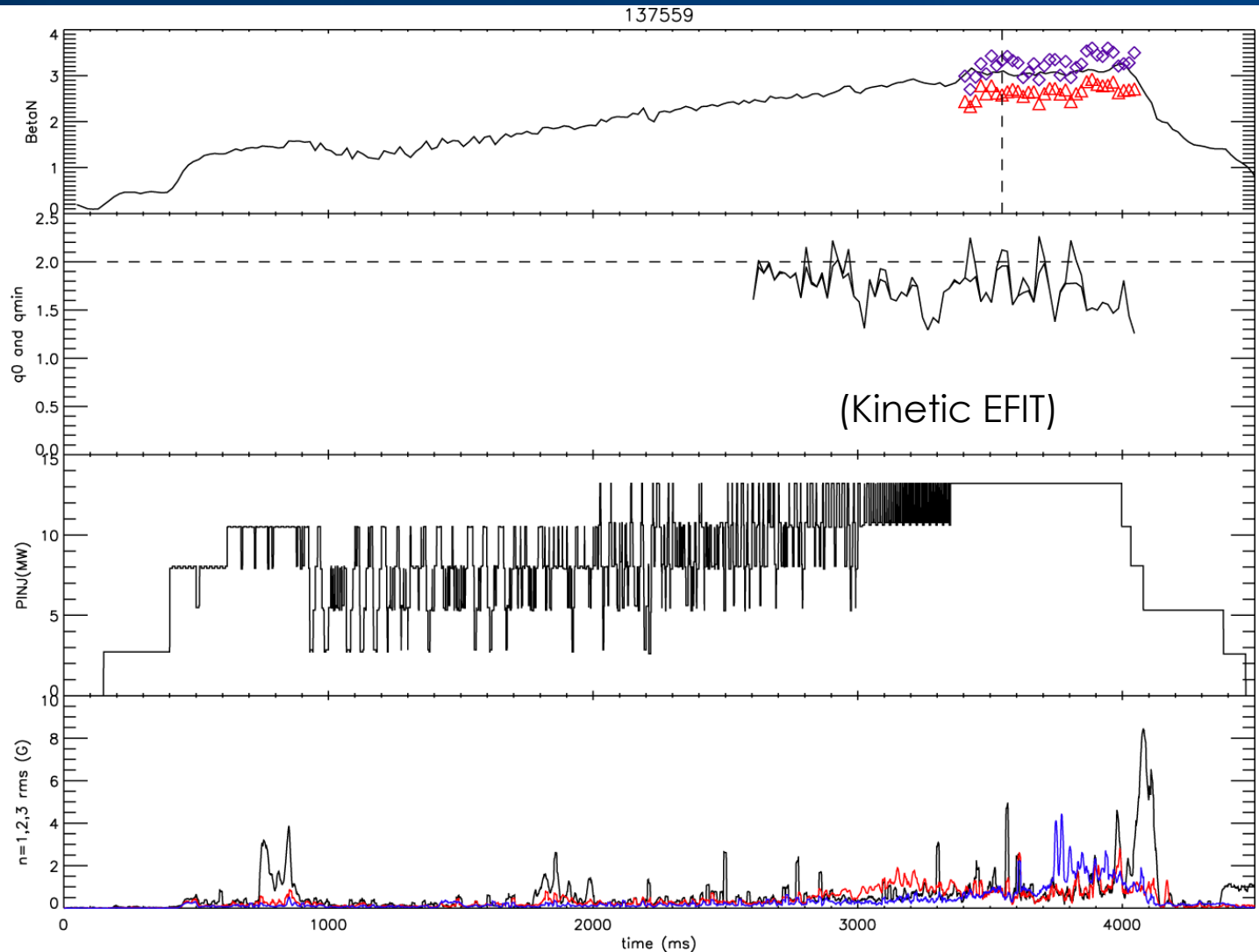
# With On-Axis NBI, it is Difficult to Maintain $\min(q) > 2$ and Achieve High $\beta_N$

2009 Shot

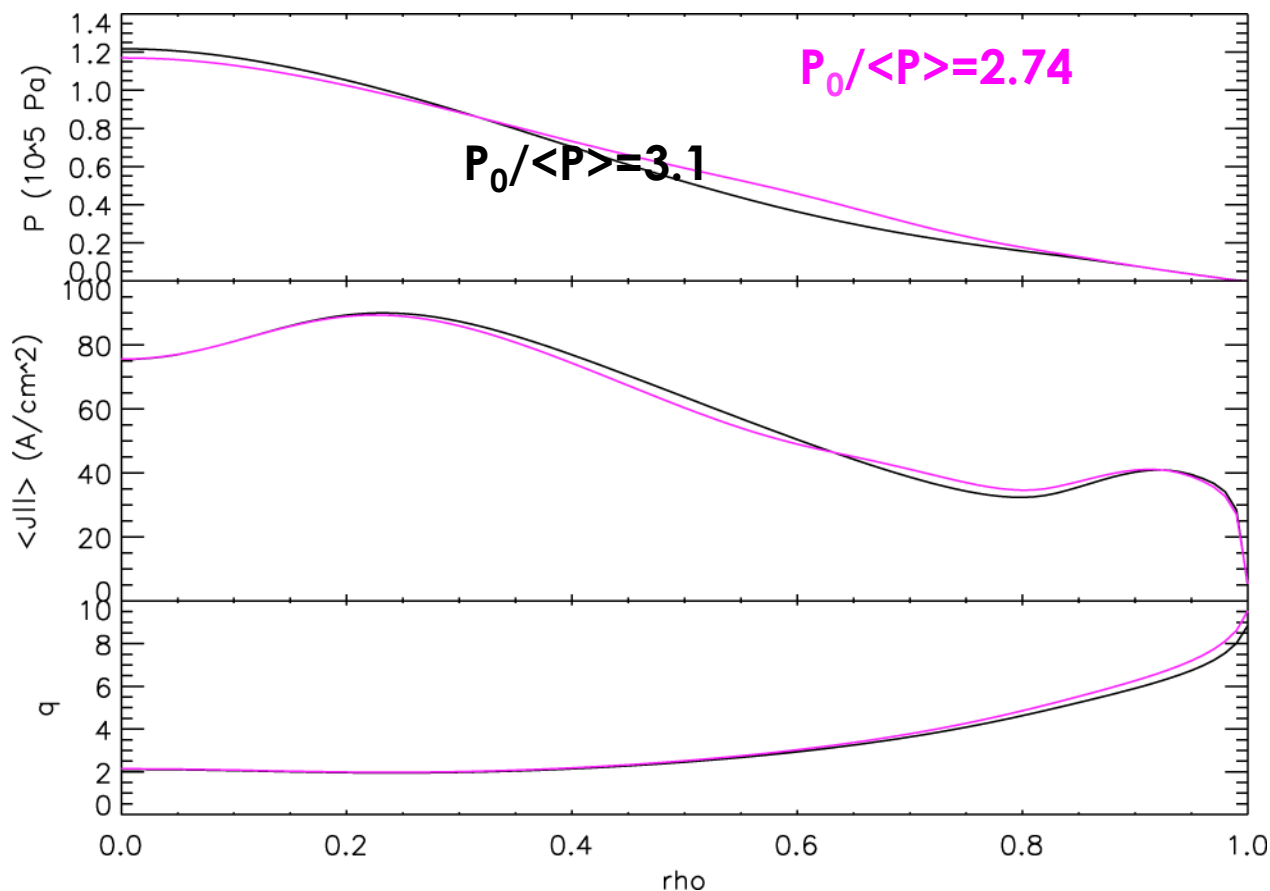
$\beta_N$  at ideal wall  $n=1$  limit

Target  $q_{\min} = 2$  not maintained

$B_T = 2$  T,  $H_{89} = 2$  require all available co-NBI power



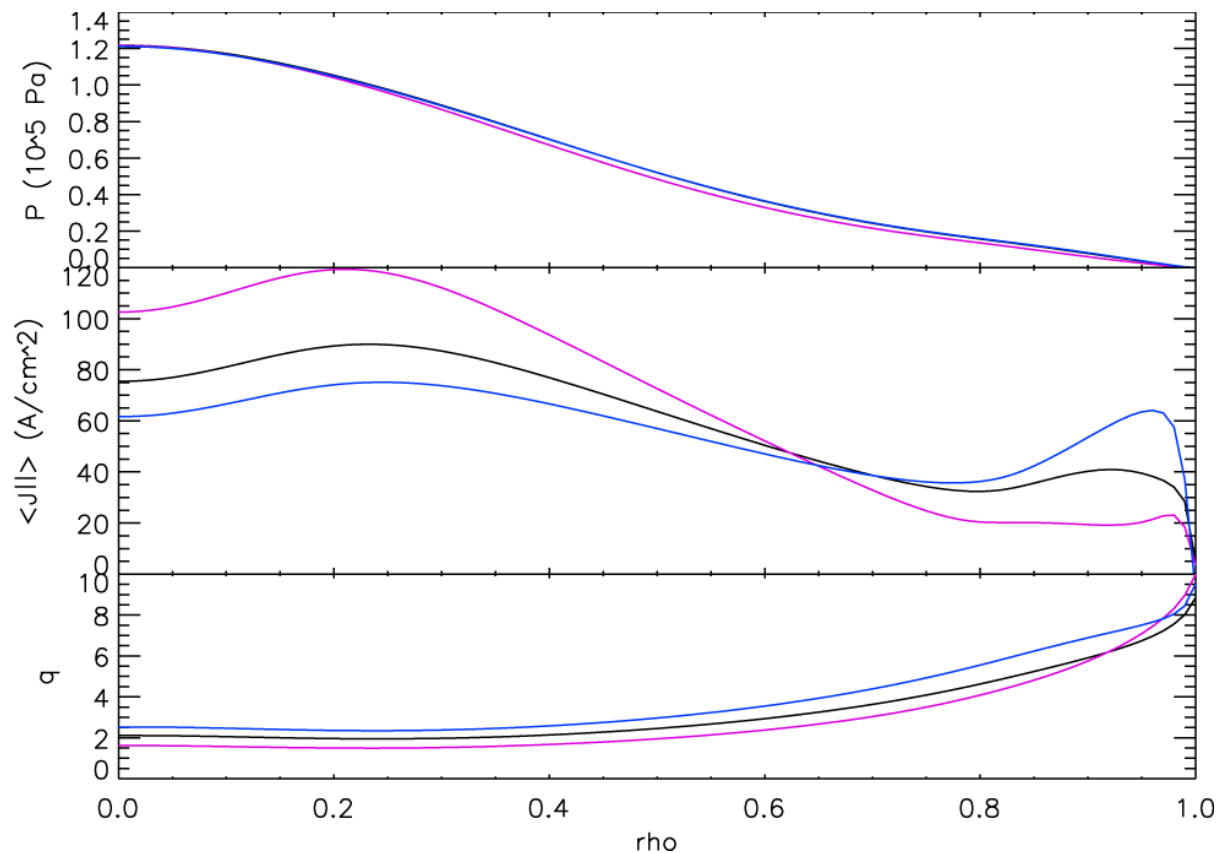
# Modeling Indicates Only Modest Gain In $\beta$ Limit by Broadening Only the Pressure Profile



- Changed P at fixed  $I_p$
- DCON results

$P_0/\langle P \rangle$	3.1	2.74
$\beta_N$ n=1 nw	2.59	2.84
$\beta_N$ n=2 nw	3.32	3.41
$\beta_N$ n=3 nw	3.66	3.61
$\beta_N$ n=1 iw	3.34	4.25
$\beta_N$ n=2 iw	3.66	3.93
$\beta_N$ n=3 iw	3.8	3.86

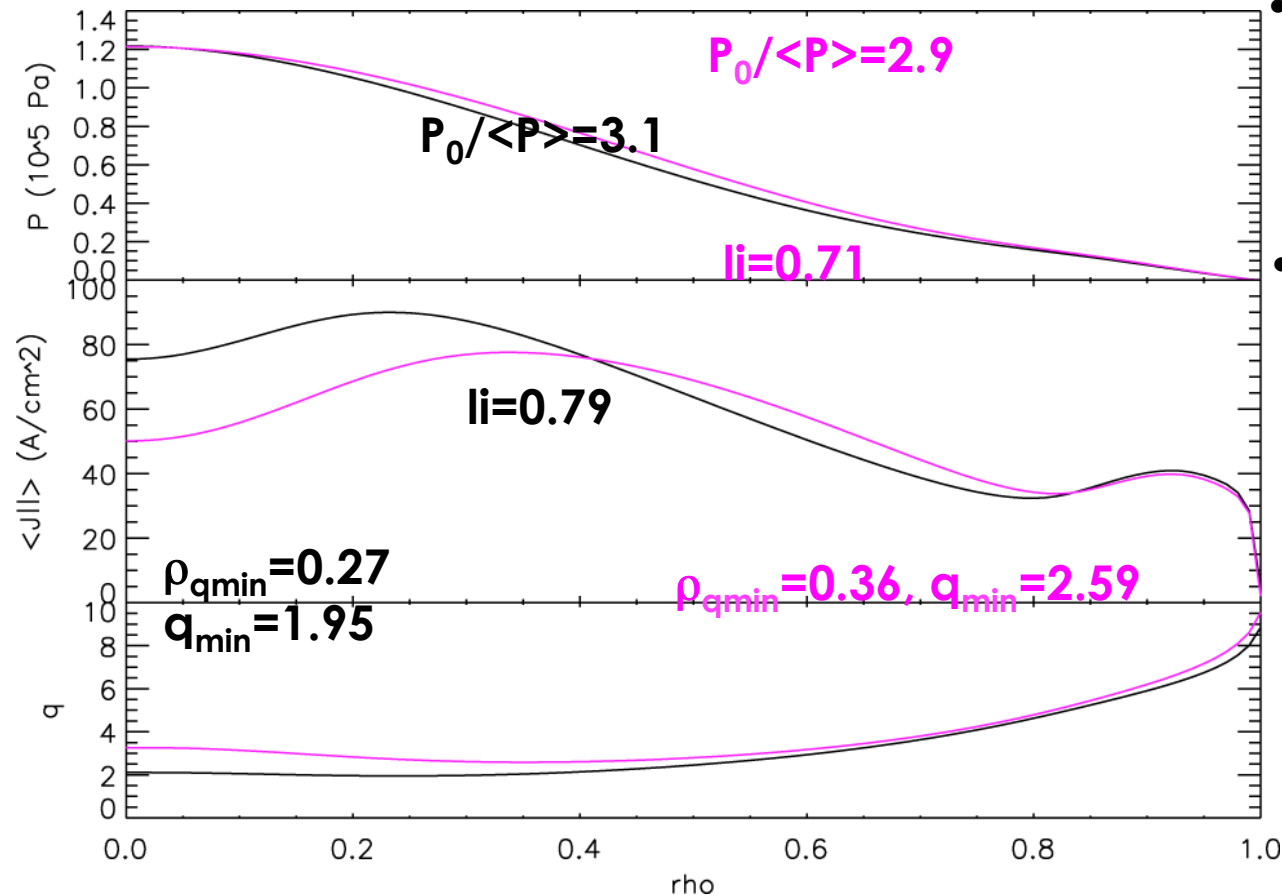
# Modest Improvement in the Calculated $\beta$ Limit by Increasing $q_{\min}$ While Holding $\rho_{q_{\min}}$ Fixed



- Scaled  $q_{\min}$  at fixed  $I_p$
- DCON results

$q_{\min}$	1.495	1.95	2.35
$l_i$	1	0.79	0.6
$\beta_N$ n=1 no-w	3.56	2.59	2.48
$\beta_N$ n=2 no-w	3.59	3.32	3.15
$\beta_N$ n=3 no-w		3.66	3.64
$\beta_N$ n=1 ideal	4.35	3.34	3.87
$\beta_N$ n=2 ideal	3.62	3.66	3.97
$\beta_N$ n=3 ideal	3.90	3.80	4.12

# Broadening J Increases the Calculated $\beta_N$ Limit Significantly

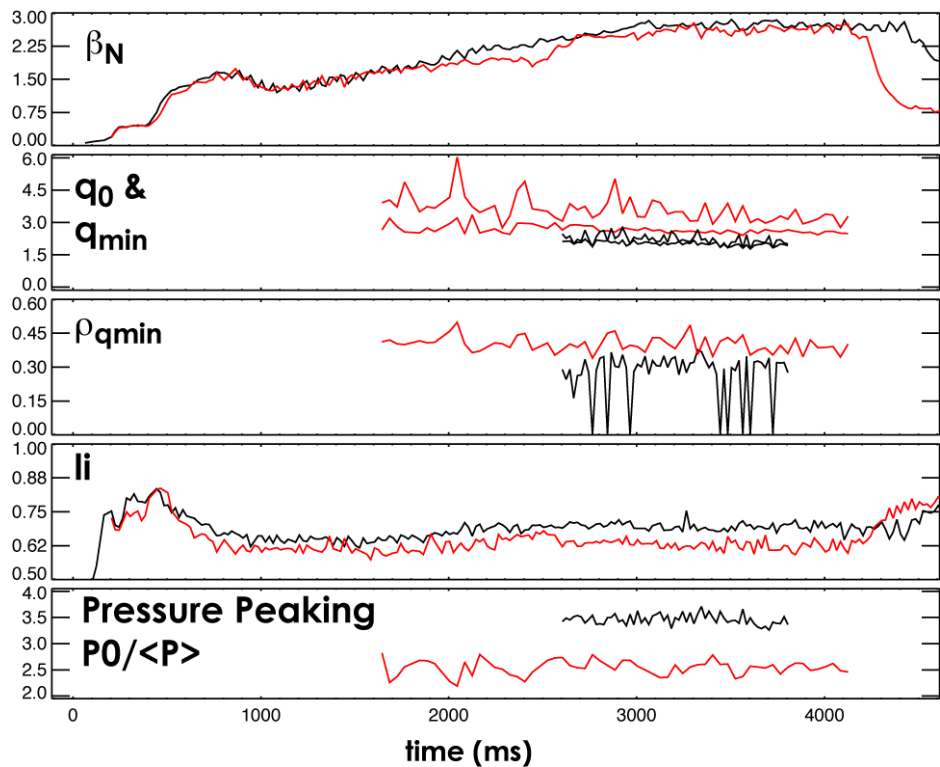


- $\Delta J_{||}$  derived from difference between simulations of NB on-axis and NB off-axis
- Fixed  $I_p$

$\beta_N$ n=1 no-wall	2.59	2.69
$\beta_N$ n=2 no-wall	3.32	3.53
$\beta_N$ n=3 no-wall	3.66	3.93
$\beta_N$ n=1 ideal-w	3.34	4.26
$\beta_N$ n=2 ideal-w	3.66	4.27
$\beta_N$ n=3 ideal-w	3.80	4.31

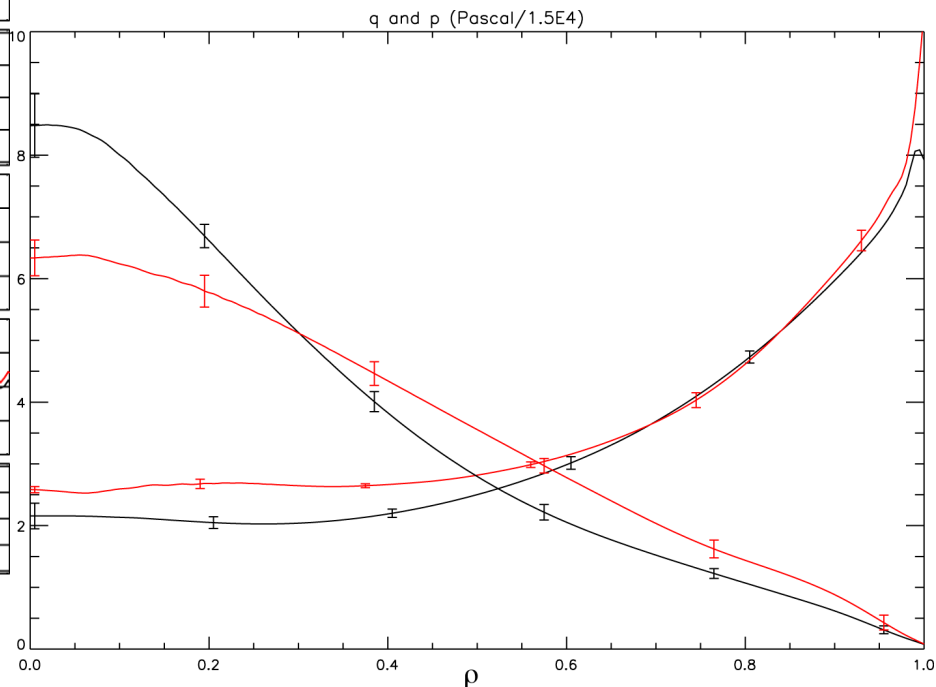
# Experimental Pressure and Current Profiles Are Broader With Off-Axis NBI and More ECCD Power

$B_T=2\text{ T}$ ,  $q_{95}=6.8$ , Matched  $\beta_N \approx 2.8$  of 2009 Reference Shot



(Kinetic EFITs)

Time Averaged Profiles in  $\beta_N$  flattop:  
With central NBI, **with off-axis NBI**

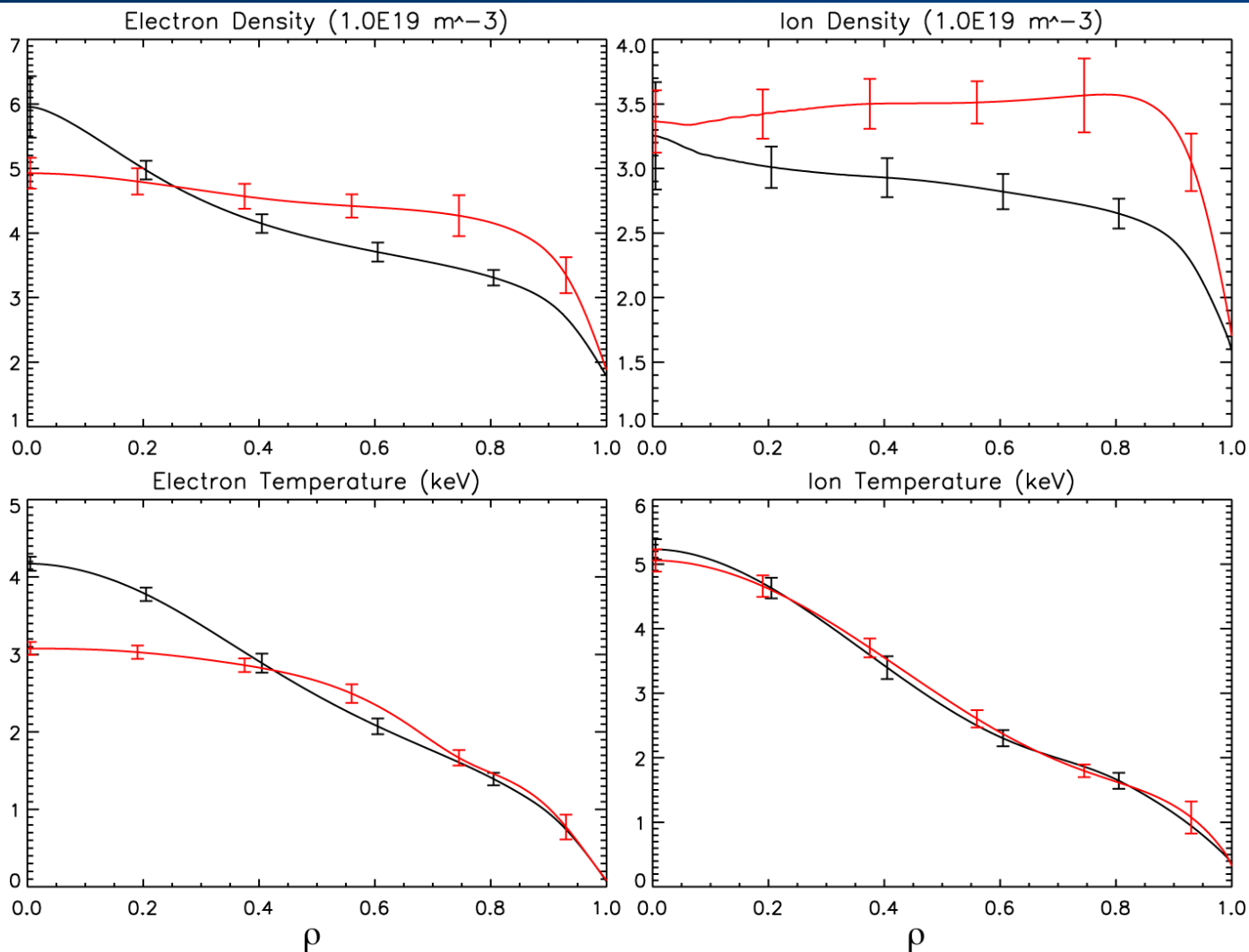




# Density and Electron Temperature Profiles Are Broader With Off-axis NBI

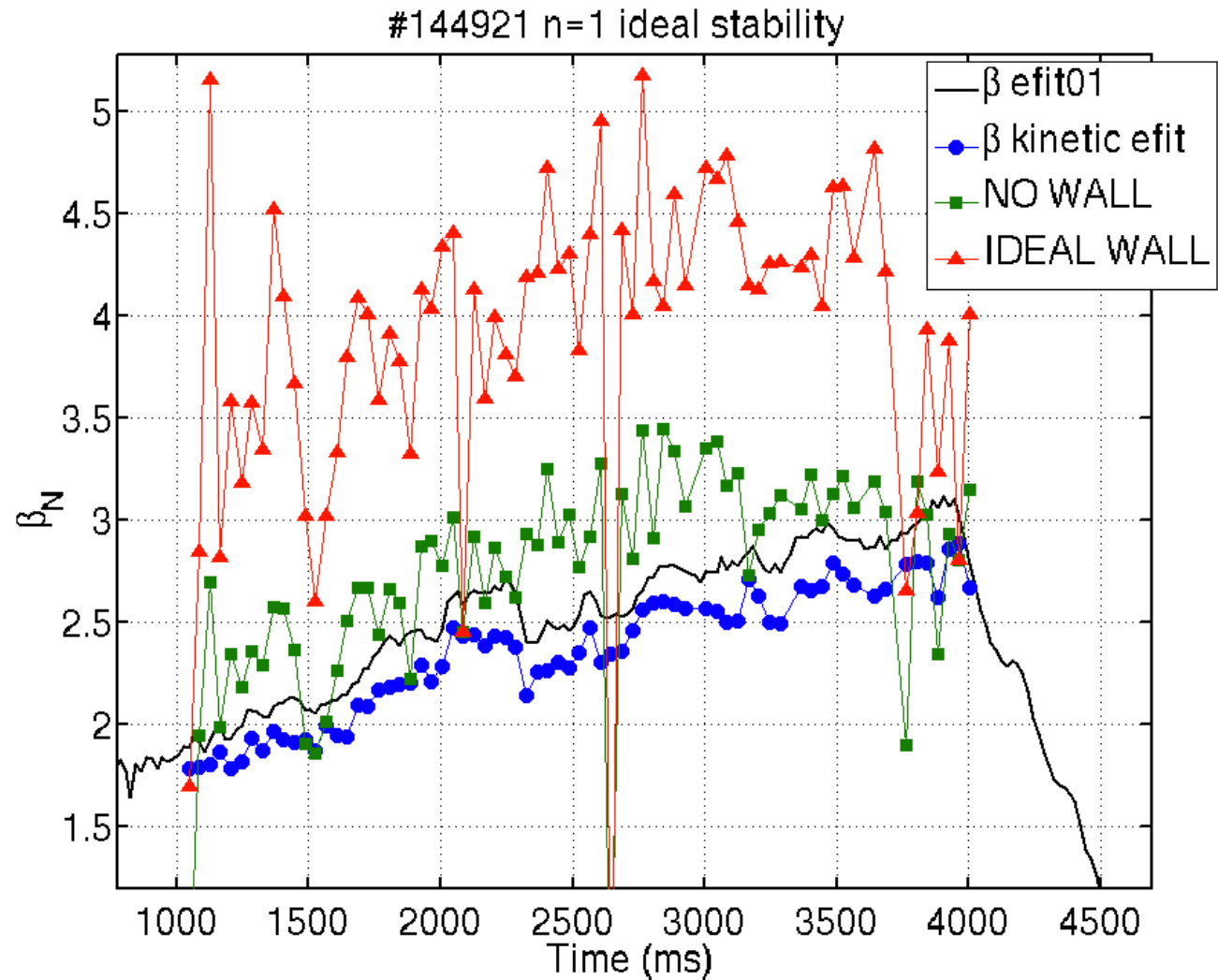
Time Averaged Profiles in  $\beta_N$  flattop

Not clear why the density profile is different



# Stability Analysis Indicates the Ideal-Wall $n=1$ $\beta_N$ Limit is Typically Over 4 With Off-axis NBI

- $\text{Min}(q) > 2$  easily sustained
- Confinement limits  $\beta$  with the available power for this B

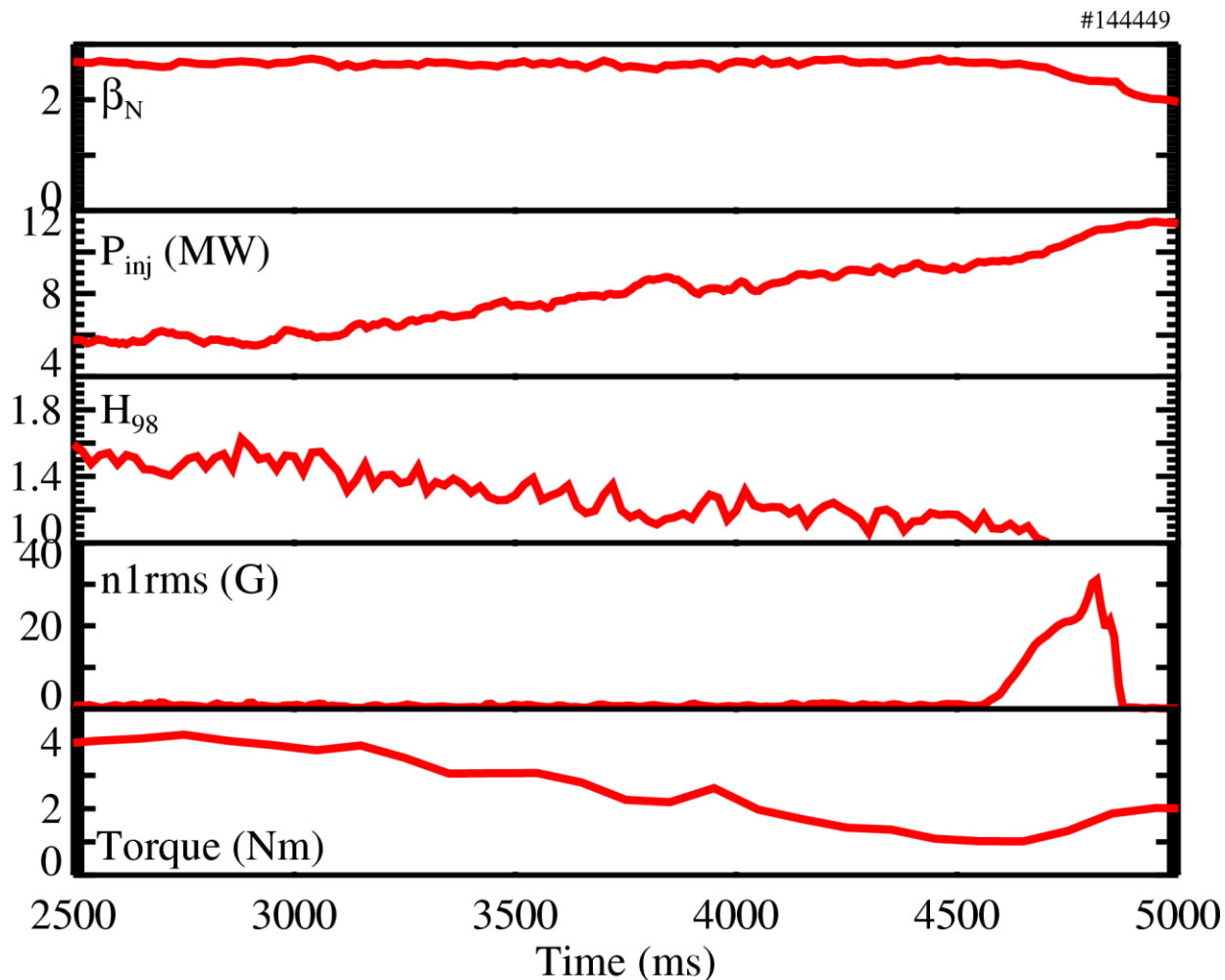


# Recent Experiments Are Pushing Advanced Inductive Regime toward Zero External Torque Input

- **Previous results with a co-NBI startup followed by a transition toward more balanced injection showed:**
  - Significant degradation of confinement as external torque was reduced
  - Lower limit on external torque set by locked mode
- **New approach taken this year to start with zero-torque or low-torque from the beginning**

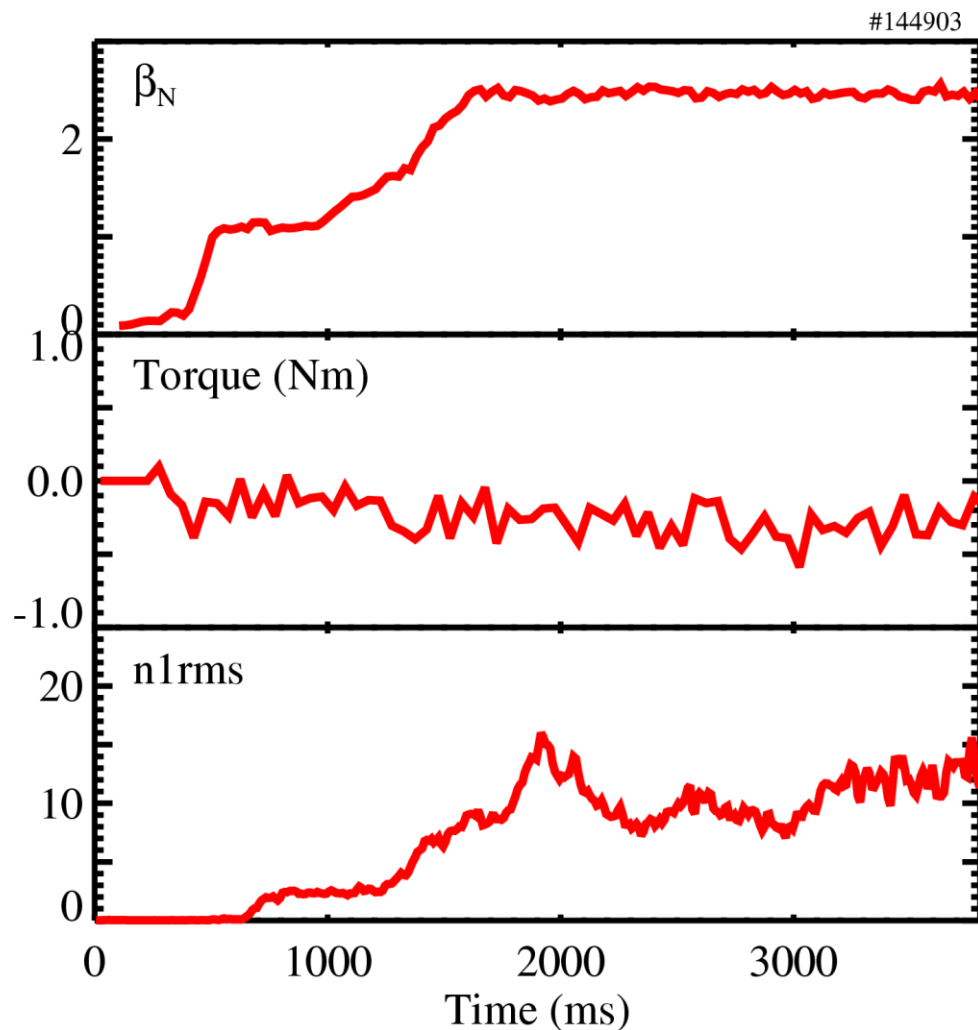
# Significant Reduction in Confinement Observed as Torque Is Reduced

- 2/1 NTM invariably encountered at low torque
- Power demand increase ~70% for fixed  $\beta_N$  (before 2/1 onset)
- H98 reduced from >1.5 to approx 1.0
- Similar to previous results  
[Politzer NF 2008]



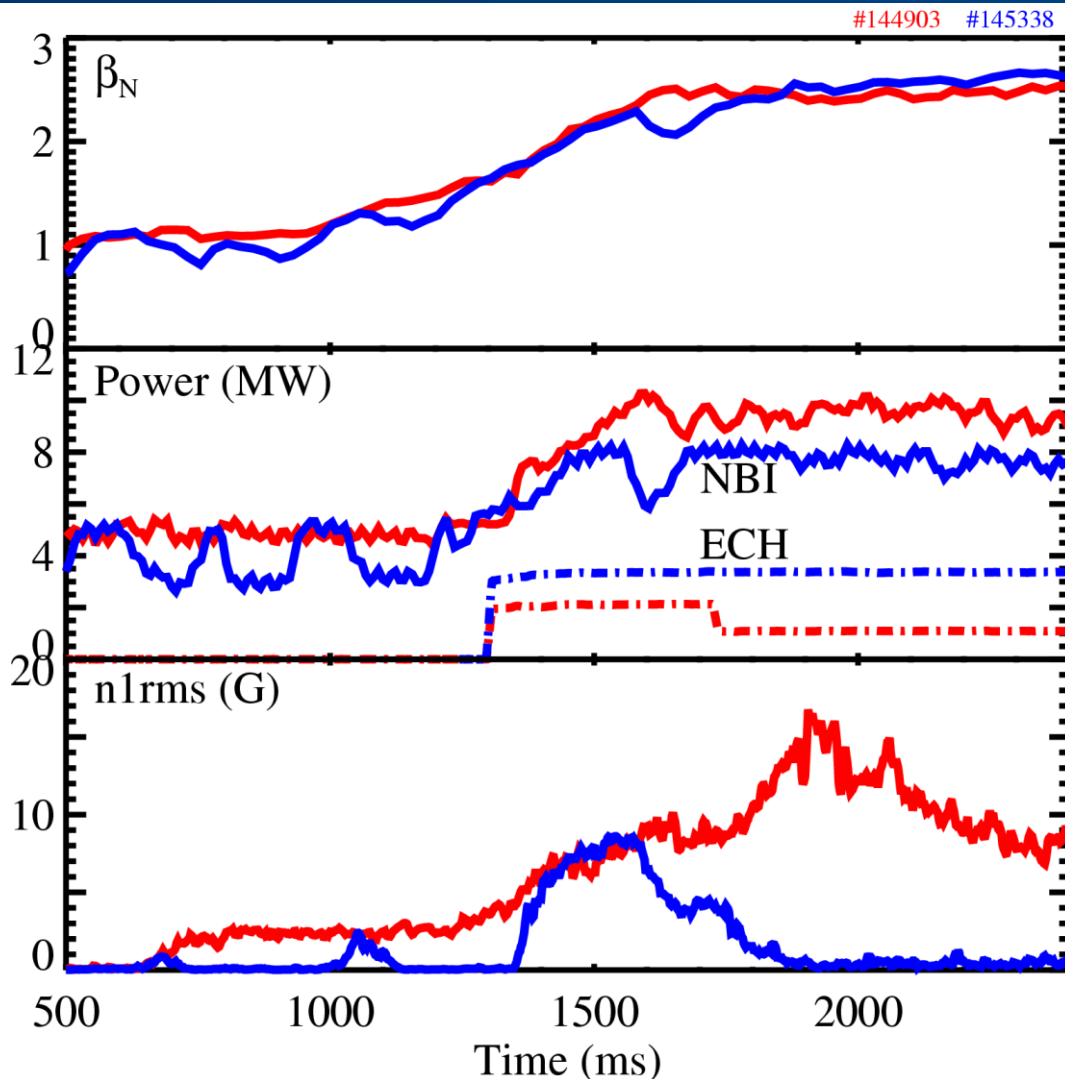
# H-mode Startup with ECCD (2 Gyrotrons) Resulted in Stable AI Discharge with Zero Net torque Throughout

- **Modest ECH power allowed 2/1 to be reduced sufficiently to allow stable operation at  $\beta_N \sim 2.5$** 
  - Unknown whether additional sources would have suppressed mode completely
  - Unknown whether plasma remains stable if remove ECCD later in discharge
- **Sustained for max duration of 210RT beam**
- **Note, no obvious 3/2 or 4/3 mode present**
  - Is this a 2/1 AI plasma?
    - In which case, what happens if actually stabilize 2/1?



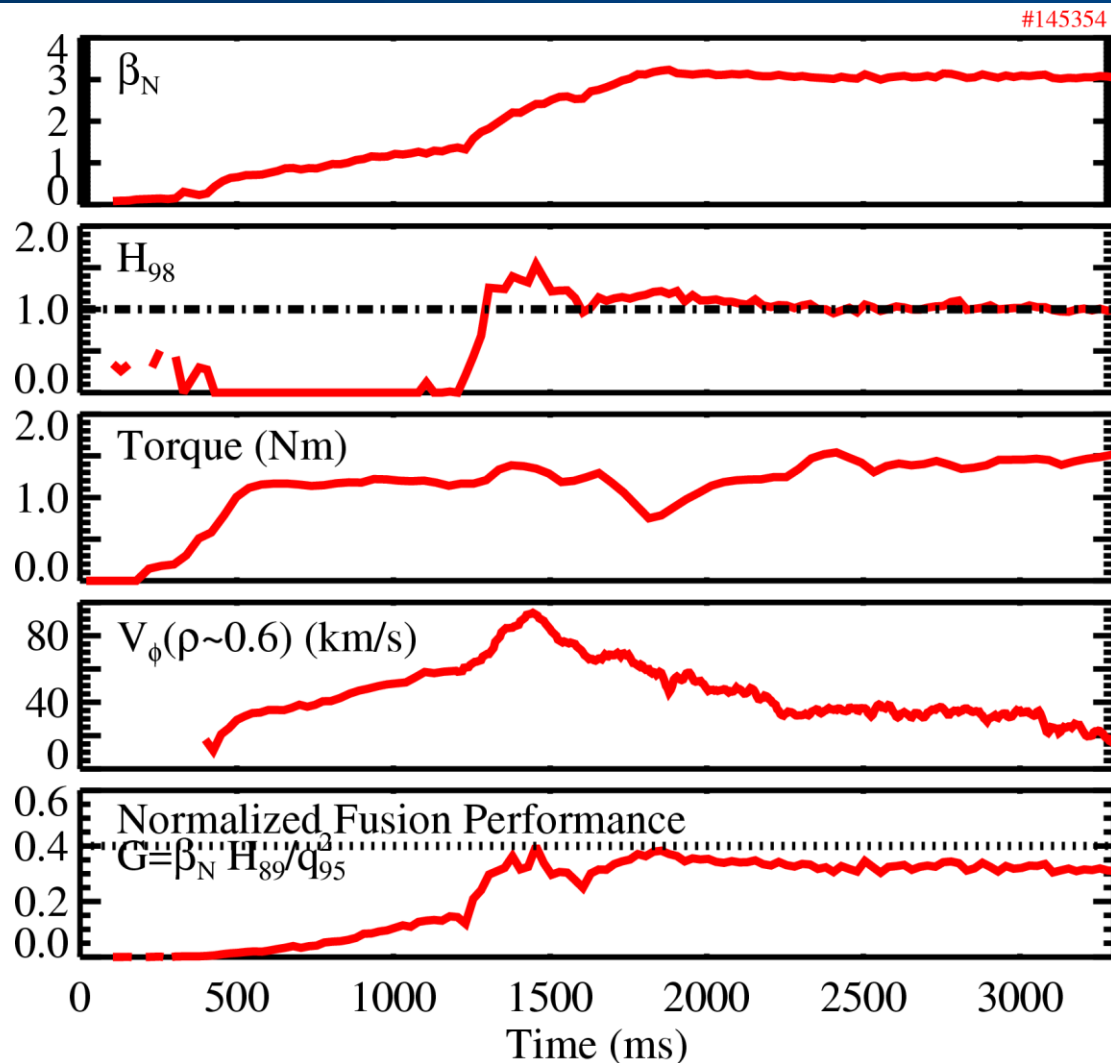
# Reproduced Low Torque Reference, and with All 6 Gyrotrons, NTM Completely Suppressed

- Slight increase in performance without 2/1 NTM, but largely offset by increased use of EC power
  - Similar  $\beta_N$  for similar combined NBI+ECH



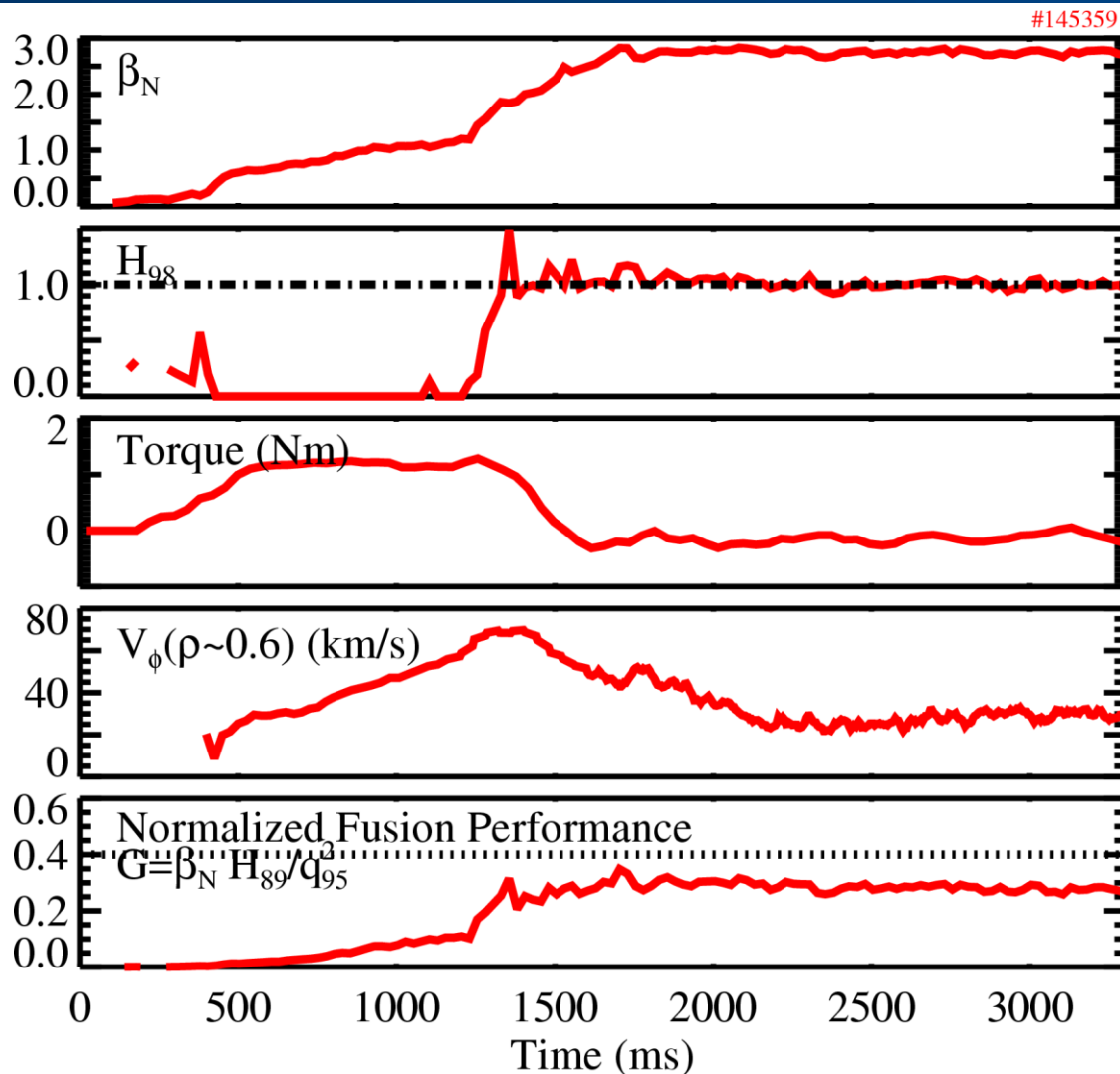
# $\beta_N \sim 3.2$ , Approaching ITER Q=10 Equivalent Achieved with Torque $\sim 1$ Nm, $H_{98} \sim 1.1$ , $G \sim 0.38$

- 1 Nm in DIII-D drives approximately the same rotation as ITER beams (30+ Nm)
  - Scaling for moment of inertia and confinement
- $H_{98} > \sim 1$
- Normalized fusion performance,  $G \sim 0.38$ 
  - $G \sim 0.4$  is ITER Q=10 equivalent



# Also Achieved Higher Fusion Performance with Net Torque~0 Nm at Higher Current, q95~4

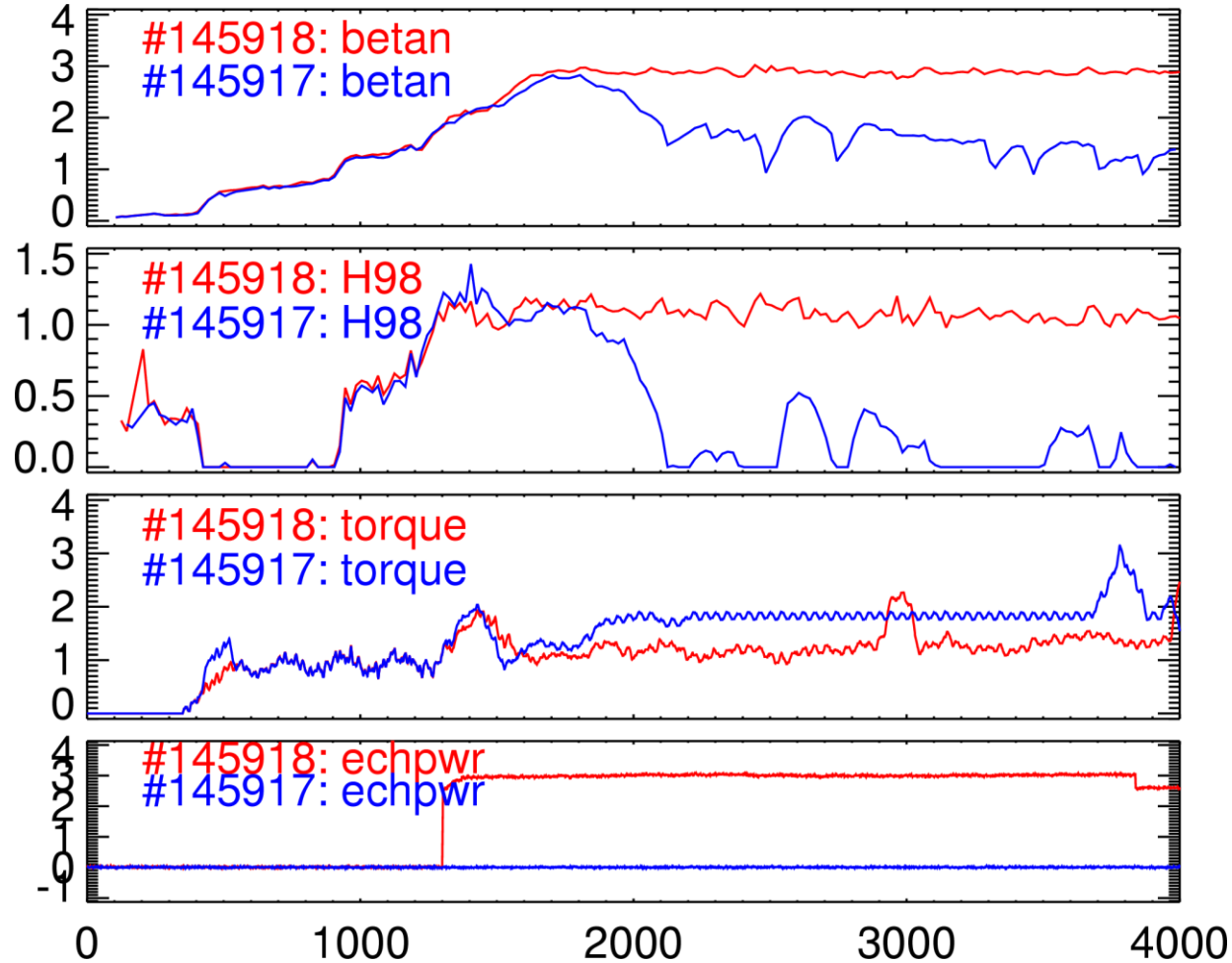
- Torque stepped down from 1 Nm in startup phase back to 0
- $\beta_N \sim 2.7$ ,  $H_{98} \sim 1$ ,  $G \sim 0.32$





# High $\beta_N \sim 3$ , Torque $\sim 1$ Nm, H98 $\sim 1$ Achieved Using Central ECH (no q=2 ECCD)

- Previous results needed ECCD at q=2 to operate at high beta and low torque
- Most recent results still required EC power, but insensitive to deposition location or heating vs current drive
  - Here,  $\rho_{ECH} \sim 0.3$  and configured for heating



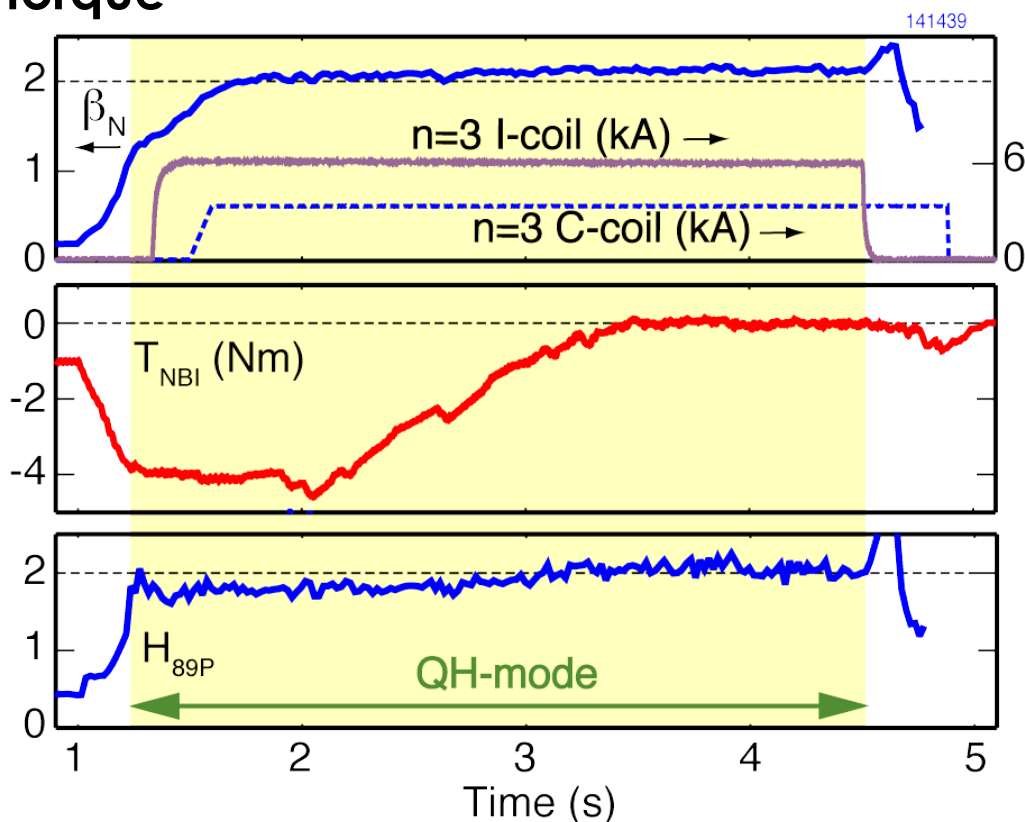
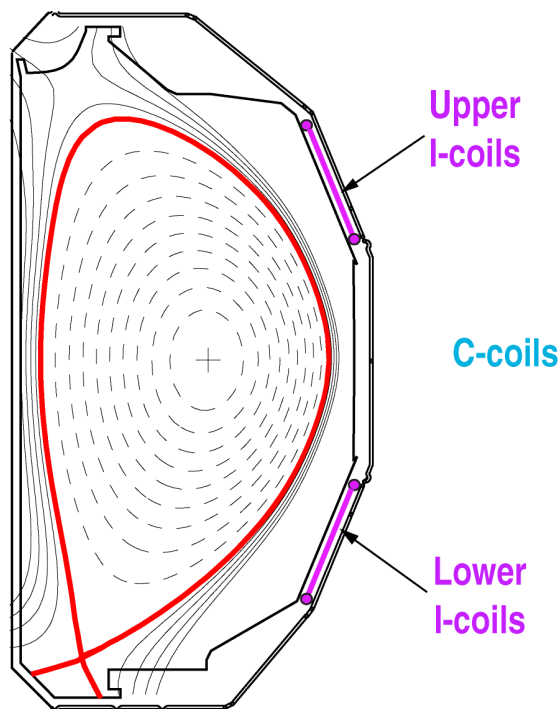
# QH Mode May Be an ITER-relevant ELM Avoidance Scheme

- **QH mode has a saturated (or stationary) edge mode instead of ELMs**
  - Observed on all 4 large divertor tokamaks
  - Traditionally observed with ctr-NBI
- **Recent results have used the plasma response to non-axisymmetric ( $n=3$ ) magnetic fields to supply the edge rotation in the counter direction believed necessary for QH mode in the absence of external torque input**

# Neoclassical Torque from 3D Fields Can Replace NBI Torque for QH-mode Access

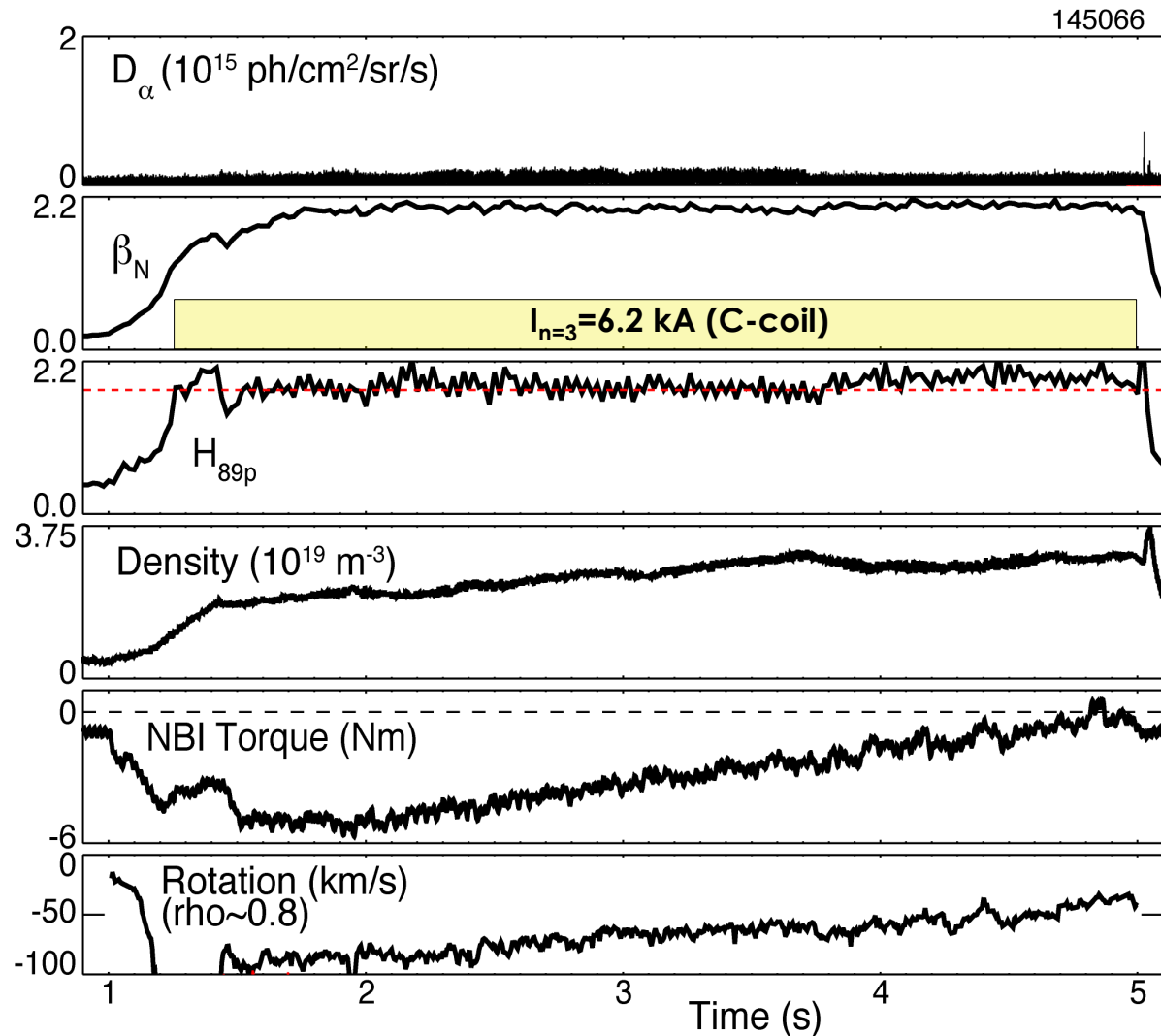
- **Previously, QH-mode required significant NBI torque**
  - Minimum pedestal velocity shear necessary for QH-mode, consistent with theory predictions [Burrell et al., PRL (2009)]
- **Counter- $I_p$  torque from nonresonant magnetic fields (NRMFs) enables QH-mode in plasmas with zero-net NBI torque**

[Garofalo et al., NF (2011)]



# Recent Experiments Aimed at Testing ITER-like NBI Torque and External Coils for 3D fields

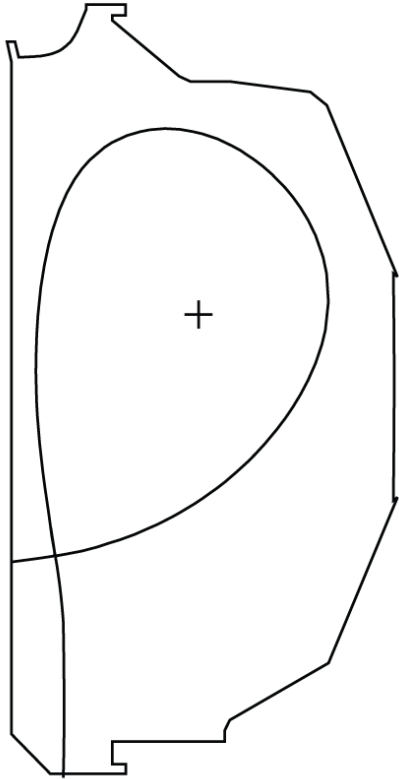
- C-coil only maintains QH-mode with zero-net NBI torque
- Confinement improves at low NBI torque
- Large counter-rotation obtained with zero-net NBI torque



# Divertor Experiments Seek to Validate Basic Scalings and Look for Impact on Pedestal and Core Performance

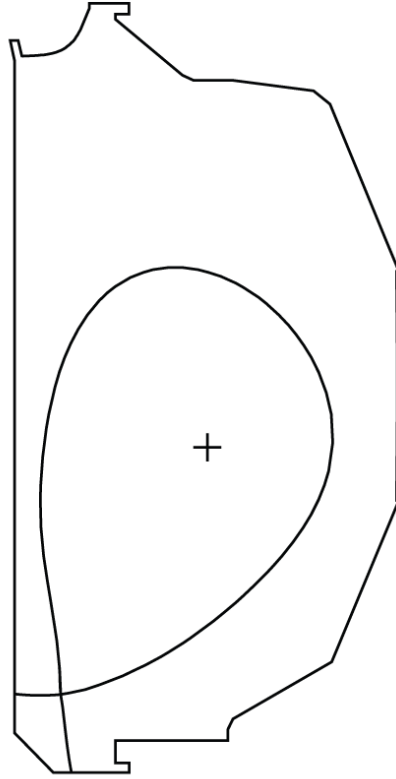
- **For fixed midplane temperature (fixed power flow?), one expects:**
  - Divertor target temperature to scale with  $1/[R_{\text{target}}]^2$  from basic geometry
  - Divertor target temperature to scale with  $1/[L_{\parallel}]^{0.57}$ , where  $L_{\parallel}$  is the parallel path length from the midplane to the divertor
- **BUT, one can turn the argument around and assume fixed divertor temperature and look for the impact on the pedestal and core parameters**

# Three Basic Shapes used in the Divertor Shaping Experiment



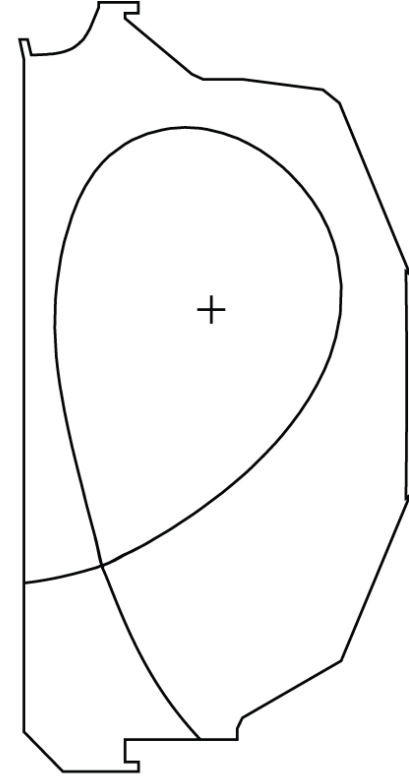
$$R_{TAR} = 1.20 \text{ m}$$

$$L_{||} (\text{mid}) \approx 40 \text{ m}$$



$$R_{TAR} = 1.21 \text{ m}$$

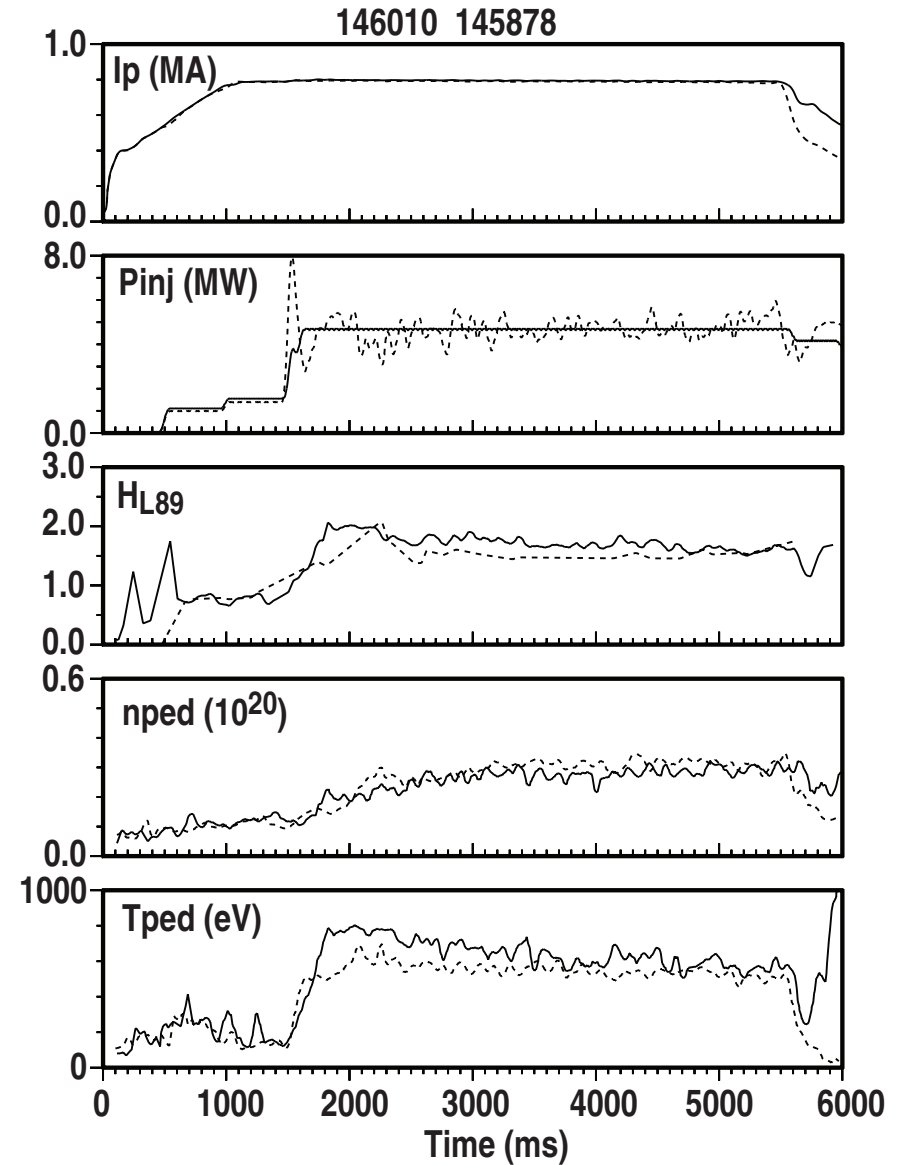
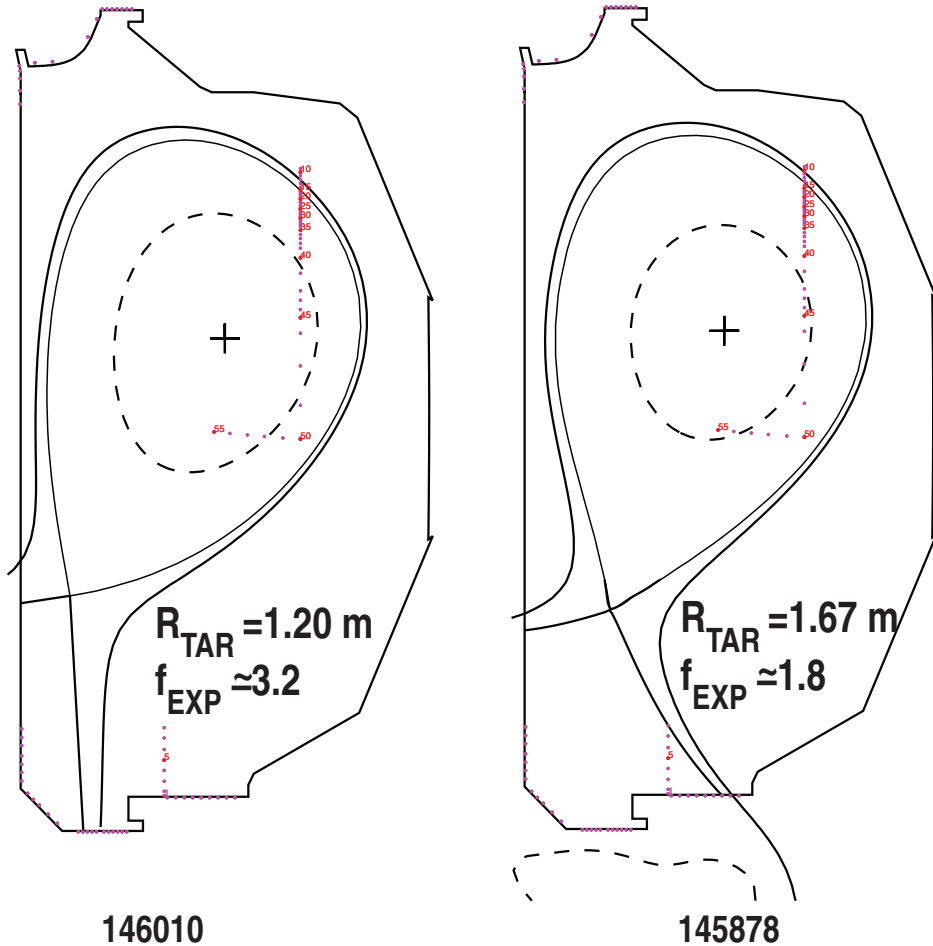
$$L_{||} (\text{mid}) \approx 32 \text{ m}$$



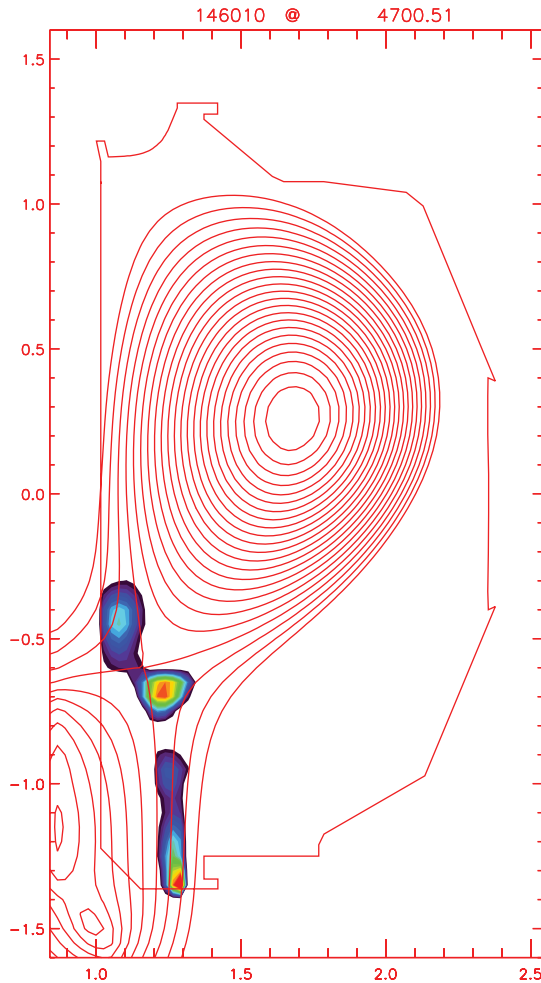
$$R_{TAR} = 1.64 \text{ m}$$

$$L_{||} (\text{mid}) \approx 36 \text{ m}$$

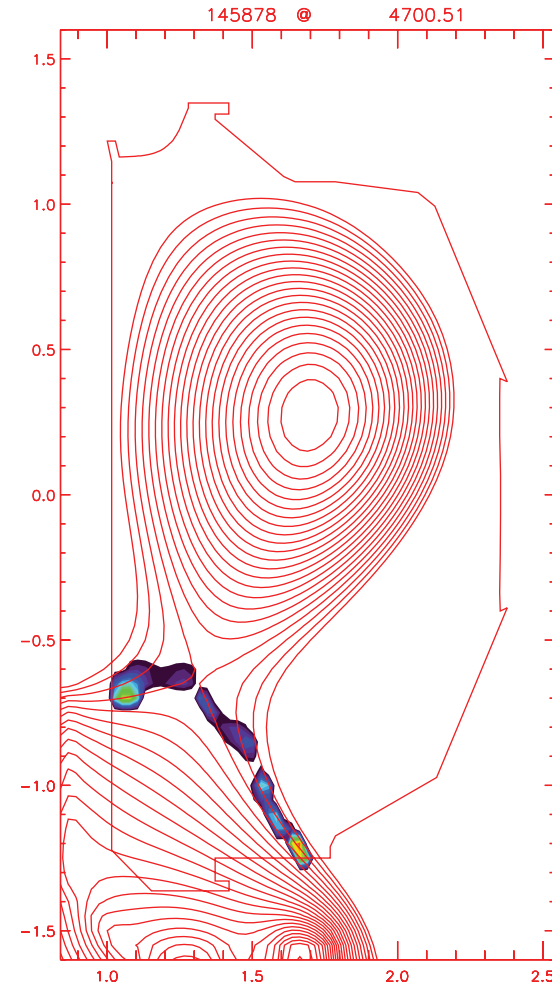
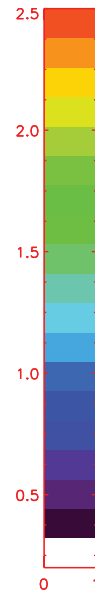
# The Base Case for the $R_{TAR}$ Comparison Have Similar Plasma Properties



# The Time-averaged Emissivity Along the Outer Divertor Leg is Markedly Different in These Attached Plasmas



$$\bar{n}_e/n_G \approx 0.35$$
$$P_{\text{RAD}}/P_{\text{IN}} \approx 0.38$$

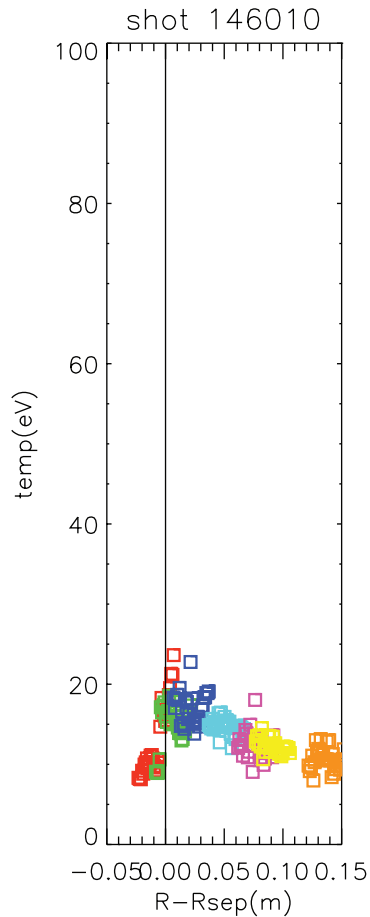


$$\bar{n}_e/n_G \approx 0.38$$
$$P_{\text{RAD}}/P_{\text{IN}} \approx 0.43$$

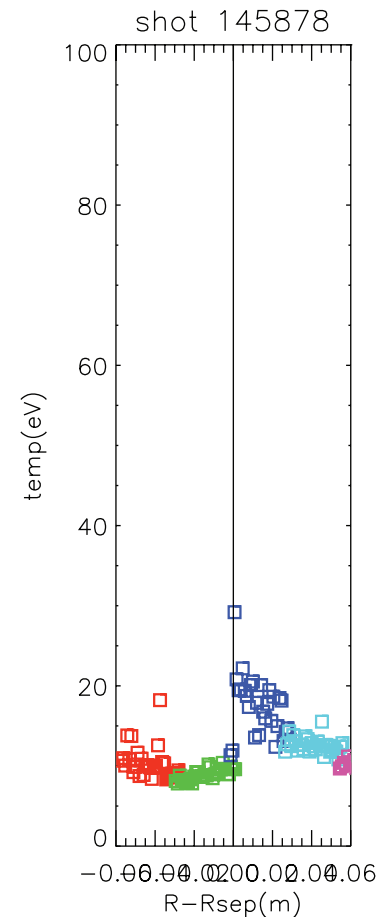
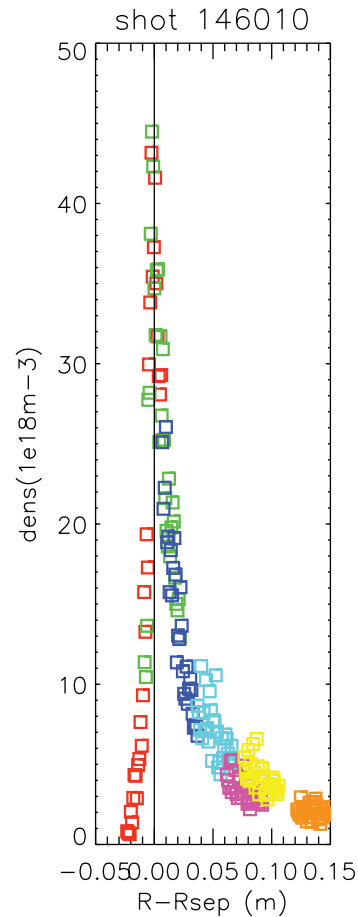


# Electron Density and Temperature at the Outer Target During H-mode Do Not Show the Expected Behaviors

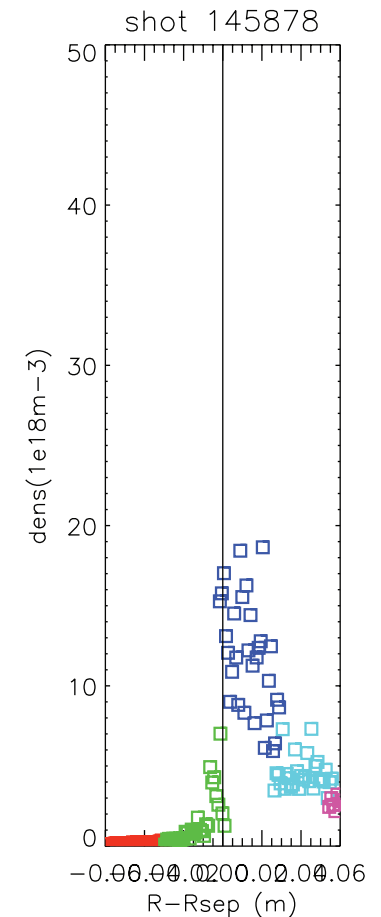
$$\left. \begin{aligned} T_{\text{TAR}} &\propto 1/R_{\text{TAR}}^2 \\ n_{\text{TAR}} &\propto R_{\text{TAR}}^2 \end{aligned} \right\} \longrightarrow \text{Expect } \sim 2\times \text{ differences}$$



$R_{\text{TAR}} = 1.20 \text{ m}$



$R_{\text{TAR}} = 1.67 \text{ m}$



# Current Profile Control Has Demonstrated Impressive Closed-Loop Results

- **Primary motivations are:**
  - Feedback control to explore suitability of target current profiles for advanced scenario operation
  - Provide reproducible target conditions to clearly distinguish effects of variations in the high performance phase
- **Two approaches were successfully demonstrated on DIII-D this year**
  - System identification approach will be discussed by Moreau in IOS-6.1 talk
  - Model-based control results discussed here

# First-principles Model-based Current Profile Control

- **Why Current Profile Control?**
  - Effect on steady-state operation, MHD stability and confinement.
- **Why Model-based Control?**
  - The high dimensionality and nonlinearity of the system dynamics, and the strong coupling between magnetic and kinetic variables, motivate the design of a model-based, multi-variable controller that takes into account the dynamic responses of both magnetic and kinetic profiles to the different actuators.
- **Why First-principles Control?**
  - The model can be expanded/modified as our system understanding improves. New physics can be easily incorporated into the model.
  - No need for a system identification experiment for each scenario of interest. Model can be more easily adapted to different scenarios.
  - The high dimensionality and nonlinearity of the system can be preserved in the model, overcoming limitations of linearized models.

# First-principles Model-based Current Profile Control

- **Our Approach to Control-oriented Modeling:**

- A first-principle model of current profile evolution in response to auxiliary heating and current drive systems (NBI, ECH, ECCD), line-averaged density and electric field due to induction was developed for an L-mode plasma.

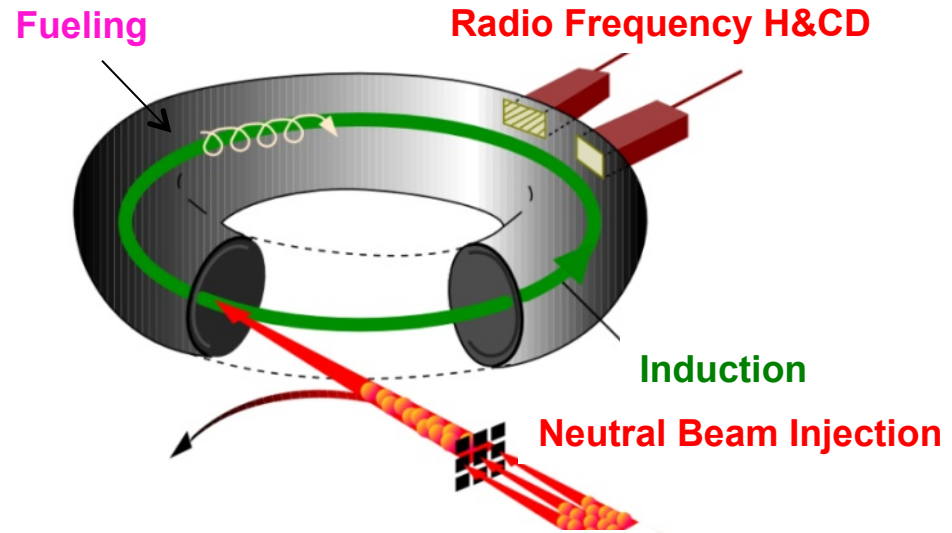
$$\frac{\partial \psi}{\partial t} = \underbrace{\frac{\eta(T_e)}{\mu_o \rho_b^2 \hat{F}^2}}_{\text{Diffusivity Control}} \frac{1}{\hat{\rho}} \frac{\partial}{\partial \hat{\rho}} \left( \hat{\rho} \hat{F} \hat{G} \hat{H} \frac{\partial \psi}{\partial \hat{\rho}} \right) + R_o \hat{H} \eta(T_e) \underbrace{\frac{(\bar{j}_{NI} \cdot \bar{B})}{B_{\phi,0}}}_{\text{Interior Control}}$$

Magnetic diffusion equation

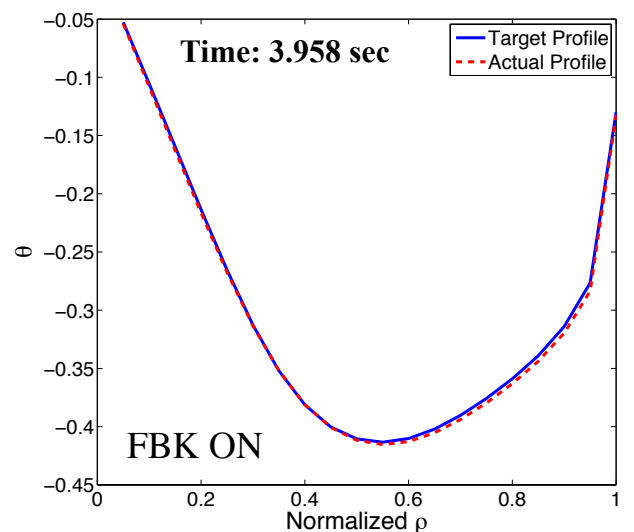
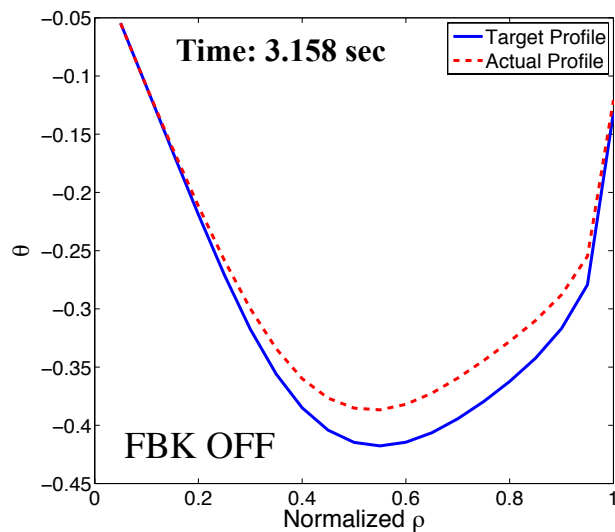
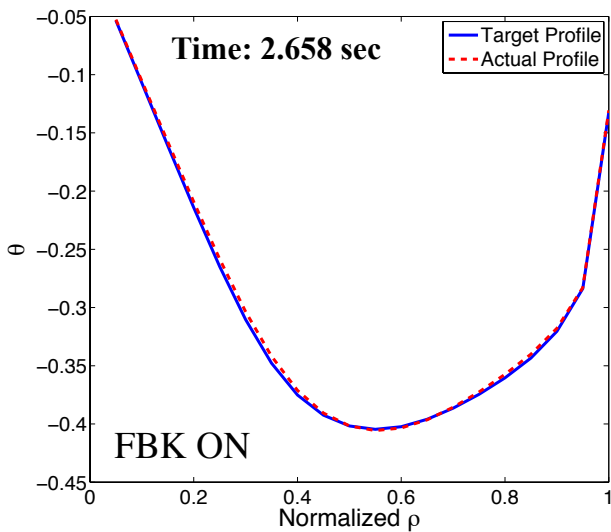
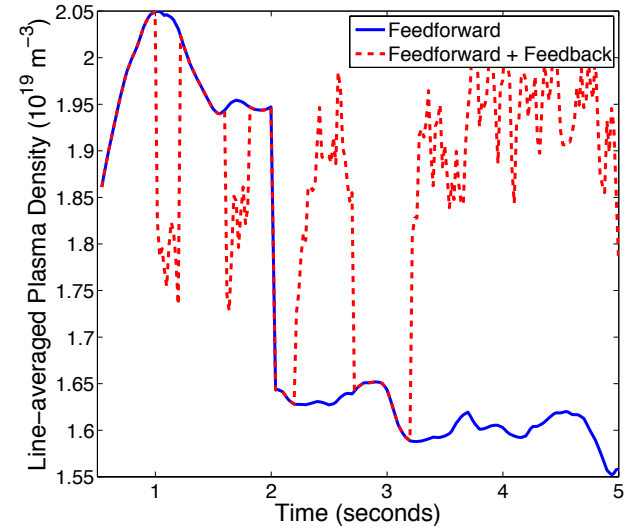
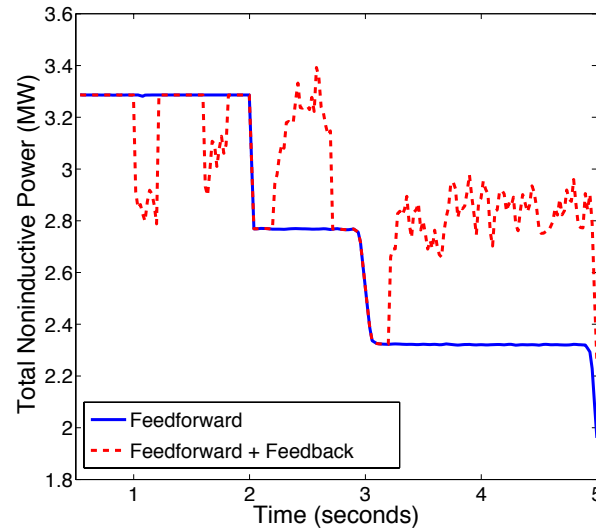
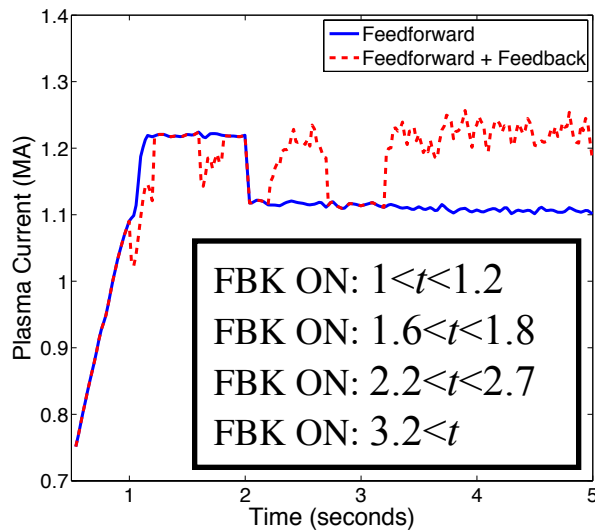
$$\left. \frac{\partial \psi}{\partial \hat{\rho}} \right|_{\hat{\rho}=0} = 0$$

**Boundary Control**

$$\left. \frac{\partial \psi}{\partial \hat{\rho}} \right|_{\hat{\rho}=1} = - \frac{\mu_o}{2\pi} \frac{R_o}{\hat{G}|_{\hat{\rho}=1} \hat{H}|_{\hat{\rho}=1}} I(t)$$



# First-principles Model-based Current Profile Control



# Plans for “October” run period

- **DIII-D management identified 3 areas of focus for this 3 week run**
  - ITER baseline scenario (especially  $n=1$  tearing stability)
  - QH mode (focus on fusion performance metric and co-NBI startup)
  - Performance extension in steady state scenario with off-axis NBI
- **Additional experiments will be done in the following areas**
  - Correction of TBM fields with coils
  - Pellet pacing of ELMs
  - Runaway channel control